

**Calibration method for carrying out multiport measurements on semiconductor wafers**

The invention relates to a method for calibrating a  
5 vectorial network analyser having n measurement ports  
and at least 2n measurement locations ( $n > 1$ ) by successive  
measurement of the reflection and transmission pa-  
rameters at different two-port calibration standards,  
which are connected between the measurement ports in  
10 any desired order and must all have a transmission  
path, and three different n-port calibration standards,  
which are connected between the measurement ports in  
any desired order and which are not permitted to show  
transmission.

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**BACKGROUND OF THE INVENTION**

Vectorial network analysers (VNA) serve for the precise  
measurement of electronic devices and components and  
20 also active and passive radiofrequency circuits and as-  
semblies through to antennas.

The so-called scattering parameters of n-ports ( $n = 1$ ,  
2, ...) are detected, which, if appropriate, are con-  
25 verted into 2n-pol-parameters (e.g. Z or Y parameters).

A so-called system error correction provides for the  
actual possibility of carrying out precise measurements  
using VNAs. In modern apparatuses, the measurement ac-  
30 curacy of VNAs is influenced almost exclusively by the  
possibility of realizing the calibration standards re-  
quired for the system-error correction.

As it is known, the reflection and/or transmission be-  
35 haviour of calibration standards, which are partly or  
completely known objects, is measured during the sys-  
tem error correction in the so-called calibration op-  
eration, at several measurement locations which are to  
optimize in position and amount.

From these measured values, correction data (so-called error variables or coefficients) are obtained by means of special computation methods. With these correction 5 data and a corresponding correction calculation, measured values from which system errors of the VNA and of the leads (instances of coupling = crosstalk, mismatches = reflections) have been eliminated are obtained for any desired measurement object.

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The customary form of description of the electrical behaviour of components and circuits in radiofrequency technology is effected by means of the scattering parameters (also called S parameters). They link wave 15 variables with one another, rather than current and voltages. This representation is particularly adapted to the physical conditions.

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The following relationship applies to - for instance - waves a1 and a2 running up to a two-port and the waves b1 and b2, which are respectively continuing in the opposite direction:

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$$\begin{pmatrix} b_1 \\ b_2 \end{pmatrix} = \underbrace{\begin{pmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{pmatrix}}_{=[S]} \begin{pmatrix} a_1 \\ a_2 \end{pmatrix},$$

wherein [S] shall be the scattering matrix identifying the two-port.

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One known calibration method for a two-port model with 10 or 12 error variables is the so-called 10-term or 12-term method. It is also referred to as SOLT (S: Short, O: Open, L: Load = Match, T: Thru) in the 35 American literature and as TMSO in Europe. It is the only system calibration method for two-port network analysers with just three measurement locations,

wherein each measurement location is located at the common measurement channel for both ports before the switch which switches each time one of the ports for measurement, and further measurement locations, which  
5 are arranged at the measurement channel of each port. But in this arrangement of the measurement locations the switch is integrated in the measurement of the calibration standards.

10 In the case of this TMSO calibration method, which is used the most often in practice, it is necessary first of all for the two measurement ports to be connected ( $T = \text{Thru}$ ). Three known one-ports, e.g. wave sink ( $M = \text{Match}$ ), Short circuit ( $S = \text{Short}$ ) and open circuit ( $O = \text{Open}$ ), then have to be contact-connected and measured  
15 at each measurement port.

The multiport measurement problem consists in the fact that all the measurement ports are coupled to one another via the measurement object. This means that it is no longer the case that a measure of the incoming wave is obtained at one measurement location, a measure of the reflective wave is obtained at the next measurement location and a measure of the transmitted wave is finally obtained at a further measurement location, independent of the terminations of the multiport, rather it is necessary additionally to take account of the reflection properties of the other measurement ports in the model.

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#### PRIOR ART

In recent years, a number of solutions have been published and patented for this multiport measurement problem. The solution to the multiport measurement problem Ferrero, described in Ferrero, Pisani, Kerwin, "A New Implementation of a Multiport Automatic Network Analyzer", IEEE Trans. Microwave Theory Tech., vol. 40, Nov. 1992, pp. 2078-2085, requires an network analyser

with likewise  $2n$  measurement locations with the same outlay on calibration standards as the TMSO method. Accordingly, the requirements made of the hardware of the calibration standards are considerably very complex.

5 Likewise, all the calibration standards have to be completely known in Ferrero's method. This is especially disadvantageous since the known standards have never been perfectly realized. Furthermore, Ferrero's method is based exclusively on the 7-term principle, so that

10 significant measurement errors result in that case since completely known standards cannot be realized perfectly and the 7-term principle reacts substantially more sensitively to such model errors, described in Heuermann, "Sichere Verfahren zur Kalibrierung von

15 Netzwerkanalysatoren für koaxiale und planare Leitungssysteme" [Reliable methods for the calibration of network analysers for coaxial and planar line systems], Dissertation document, Institute for Radiofrequency Technology, Ruhr-University Bochum, 1995, ISBN 3-8265-

20 1495-5.

The 10-term methods according to DE 199 18 697 A1 requires just  $n+1$  measurement locations but only known calibration standards.

The multiport 7-term methods according to DE 199 18 960 A1, which build on an adaptation of the known two-port methods to a multiport method, comprise the methods

30 TAN, TNA, LAN, TRL, TLR, LLR, LRL, TAR, TMR, TRM, TMS, LMS, TMO, LMO, UMSO, TMN, LNN, TZU, TZY, TYU, LZU, ZZU, YYU, QSOLT and generally require only  $n-1+2$  calibration measurements.

35 A further method from the company ATM is described in the American Patent Specification US 5578932. The patent specification describes in detail a so-called test set which can be used to extend a 2-port network analyser to  $n$  ports. Furthermore, a special calibration

device is described, which is required for the automatic calibration of the said test set.

The calibration device contains, in addition to the standards open, short and match (also termination), an arrangement of different transmission lines which can be connected between the terminals of the calibration device via semiconductor switches. Consequently, as in the TMSO method, all the standards must be completely known. In contrast to the statement in the Abstract, however, complete multiport calibration and error correction does not take place. Instead, only two-port paths are calibrated; the remaining ports are not taken into account (column 18, line 57). Two-port measurements are carried out successively during later measurement operation. In this case, the measurement ports that are not included in the calibration are successively terminated by different reflection standards incorporated within the test set. Precisely one 2-port measurement is carried out for each value of the reflection standard (column 21, line 1). Once the measurements have been carried out at all measurement ports, a result corrected with respect to the systematic errors can be calculated from the measured values obtained and the known values of the reflection standards. According to the patent specification, the measurement of a 3-port test object requires 2 two-port measurements from port 1 to port 2 and from port 1 to port 3 (column 21, line 1 and line 45), in which case, for complete characterization of all the parameters, it is necessary to terminate the third port of the test object that was not included, during the measurement from port 1 to port 2, by at least 3 different reflection standards (column 21, line 28). This means that the complete characterization of a 3-port requires  $3 + 1 = 4$  two-port measurements, while the method presented here manages with 3 two-port measurements.

Moreover the measurement of electronic devices on wafer underlies certain boundary conditions especially with regard to the possibility of realisation of calibration 5 standards.

In the semiconductor field, it is not unusual for users to realize the calibration standards of the wafers themselves. The geometrical reproducibility and equal- 10 15 20 25 30 35 40 45 50 55 60 65 70 75 80 85 90 95 100 105 110 115 120 125 130 135 140 145 150 155 160 165 170 175 180 185 190 195 200 205 210 215 220 225 230 235 240 245 250 255 260 265 270 275 280 285 290 295 300 305 310 315 320 325 330 335 340 345 350 355 360 365 370 375 380 385 390 395 400 405 410 415 420 425 430 435 440 445 450 455 460 465 470 475 480 485 490 495 500 505 510 515 520 525 530 535 540 545 550 555 560 565 570 575 580 585 590 595 600 605 610 615 620 625 630 635 640 645 650 655 660 665 670 675 680 685 690 695 700 705 710 715 720 725 730 735 740 745 750 755 760 765 770 775 780 785 790 795 800 805 810 815 820 825 830 835 840 845 850 855 860 865 870 875 880 885 890 895 900 905 910 915 920 925 930 935 940 945 950 955 960 965 970 975 980 985 990 995 1000 1005 1010 1015 1020 1025 1030 1035 1040 1045 1050 1055 1060 1065 1070 1075 1080 1085 1090 1095 1100 1105 1110 1115 1120 1125 1130 1135 1140 1145 1150 1155 1160 1165 1170 1175 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2180 2185 2190 2195 2200 2205 2210 2215 2220 2225 2230 2235 2240 2245 2250 2255 2260 2265 2270 2275 2280 2285 2290 2295 2300 2305 2310 2315 2320 2325 2330 2335 2340 2345 2350 2355 2360 2365 2370 2375 2380 2385 2390 2395 2400 2405 2410 2415 2420 2425 2430 2435 2440 2445 2450 2455 2460 2465 2470 2475 2480 2485 2490 2495 2500 2505 2510 2515 2520 2525 2530 2535 2540 2545 2550 2555 2560 2565 2570 2575 2580 2585 2590 2595 2600 2605 2610 2615 2620 2625 2630 2635 2640 2645 2650 2655 2660 2665 2670 2675 2680 2685 2690 2695 2700 2705 2710 2715 2720 2725 2730 2735 2740 2745 2750 2755 2760 2765 2770 2775 2780 2785 2790 2795 2800 2805 2810 2815 2820 2825 2830 2835 2840 2845 2850 2855 2860 2865 2870 2875 2880 2885 2890 2895 2900 2905 2910 2915 2920 2925 2930 2935 2940 2945 2950 2955 2960 2965 2970 2975 2980 2985 2990 2995 3000 3005 3010 3015 3020 3025 3030 3035 3040 3045 3050 3055 3060 3065 3070 3075 3080 3085 3090 3095 3100 3105 3110 3115 3120 3125 3130 3135 3140 3145 3150 3155 3160 3165 3170 3175 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Therefore it is an object of the invention to propagate a method for calibrating a vectorial network analyser having  $n$  measurement ports and at least  $2n$  measurement

## 35 SUMMARY OF THE INVENTION

locations used for multiport measurement which permits a calibration with increased precision and considerable reproducibility of measurement.

5 What is disclosed as the invention is a method for calibration characterized in the calibration measurement according to Claim 1 a) up to d) and calculation of the reflection accounts of the n-one-ports according to Claim 1 e). In the following (???) the method according to Claim 1 shall be called RRMT method.

10 The RRMT method is characterized by the measurement of two reflection standards, which are similar to short circuits and to open circuits, in addition to the measurements of n impedance standards at the n-fold one-port. With that the RRMT method as well as the method according to Claims 2, 3 and 4 afford the advantages that the calibration standards do not have to be exactly known. Consequently the multiport measurements 15 can be carried out with high precision and low costs with these methods by using calibration standards which are produced from the customer. All the methods are 20 characterized by the following criterias of the calibration standards:

25 1.: The phase of the reflection standards R has to be known only to  $\pm 90^\circ$ . More information is not required. In practice, a real short circuit and a open circuit are used. The divergences to an ideal short circuit or 30 open circuit have no influence on the measurement accuracy.

2.: The impedance standards M do have to be completely known. The latter may be different, however, in the 35 case of the RRMT method. Such standards are often also referred to as transfer match.

3.: The line standard T in the case of RRMT method according to Claims 1 and 2 and also the line standard L

in the case of LRRM according to Claims 3 and 4 has to be completely known, but may have a finite attenuation and, if appropriate, a known reflection behaviour. It is also possible to use different line standards between different measurement ports.

The use of the 10-term method for the calculation of the error coefficients of the measured two-port calibration standards and of the scattering matrix is particularly advantageous in combination with other features of RRMT method due to the 10-term method is less sensitive to model errors.

Another advantage of the RRMT method is that the precision of the measurement is substantially increased compared to the prior art due to the fact that the calibration measurements of  $n$  impedance standards are carried out at one  $n$ -one-port. Deviations of properties compared to the measured reference port are so avoided at the so-called matching point ( $S_{11} = 0$ ) where the properties of the  $M$  standard are only "overcalculated". The additional measurements at the  $n$ -one-port compared to the measurements at the one-port are not disadvantageous since they proceed fully automatically to a considerable extent in the case of on-wafer measurements and their costs are a small portion of the costs of the system. Moreover these measurements provide additional information for increasing of the quality of the calibration method.

Also the RRMT methods and the methods according to Claims 2 to 4 are distinguished by the fact that they all use lines for the connections of the measurement ports. This is a particularly fact in on-wafer measurements, in contrast to coaxial measurements, where the measurement ports (on-wafer measuring tips (probes)) cannot be directly connected. Therefore, it is never possible to use a genuine Thru standard in on-wafer methods.

The normal and inevitable fluctuations in known DC impedances do not influence the methods of this invention.

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When VNAs having  $2n$  measurement locations are used, these methods of the invention operate significantly more precisely and with greater long-term stability compared to VNAs having  $n-1$  measurement locations because 10 cause drift effects of the electronic changeover switches have no influence on the measurement quality.

Also the method according to the attributes of Claim 2 make it possible to use reflection standards which does 15 not have to exactly known. Moreover the calibration measurements according to this method are carried out with high precision since the impedance standards are measured at the n-one-port.

20 The method according to Claim 2 is particularly used for multiport measurements with  $n>2$ . That is because the method uses the 7-term method for calculation of error coefficients and scattering matrix what reduces the calculational complexity and because the thru- 25 standard is measured between a reference port and other  $n-1$  ports instead between all combinations of the ports. In the following this method shall be called multiport-RRMT method or GRRMT method. The increased sensitivity of the 7-term method with regard to the 30 model errors do not have influence since the measurement of impedance is carried out at n-one-port so that an "overcalculating" is not necessary and because the 7-term method is an optimization of the calculational complexity for these multiports. The described advantages 35 in circuit and in measurement of the RRMT method also characterize the multiport-RRMT method.

Alternatively to the RRMT and GRRMT methods it is possible that for the multiport measurements with  $n>2$  the

calibration measurement according to Claims 1 b) and 2 b) is carried out at an one-port instead at a n-one-port and the properties of this impedance at the other n-1 one-ports are calculated from this calibration 5 measurement. These embodiments of the invention in the following shall be called LRRM method and GLRRM or multiport-LRRM method. In both methods the calculational complexity and the complexity in circuit and in measurement are optimized with regard to the required precision of measurement.

The four methods which are applied for under Claims 1 to 4 in this invention differ in implementation only by 10 nuances, but these nuances can have a significant effect in practise. The greatest difference is between the RRMT and GRRMT methods under Claims 1 and 2 and the multiport LRRM methods under Claims 3 and 4. In the multiport LRRM methods, only one match standard is contact-connected at a reference port and measured. 15 Whereas, both RRMT methods use an impedance standard which is contact-connected and measured at each port and which does not have to equate with any other impedance standard.

20 The difference between the two RRMT and multiport LRRM methods resides in the number of T and L measurements, respectively. The methods according to Claims 1 and 3 require k measurements, and thus more than required by the methods according to Claim 2 and 4 which requires n-1 measurements. The methods according to Claims 1 and 30 3 are in turn distinguished by a greater robustness. Thus, it can be shown e.g. that the transmission measurement dynamic range in the case of methods 1 and 3 corresponds to that of the apparatus. These methods are used when the measurement dynamic range of the network 35 analyser has to be achieved. On the other hand, the methods according to Claims 2 and 4 exhibit a significantly greater sensitivity with regard to small contact-connection errors and incompletenesses in the

calibration standards. Consequently, the methods according to 2 and 4 will be used only if the number n of measurement ports is disproportionately large.

5 With such low demands made of the calibration standard, the multiport calibration method according to the invention can also be used excellently for automated calibrations of VNAs in coaxial environments. Algorithms and associated switching networks are already  
10 marketed by a number of manufacturers for two-port calibrations. In multiport calibrations, the number of contact-connections of the calibration standards is appreciably larger, which costs time and money and entails greater risks of errors.

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#### BRIEF DESCRIPTION OF THE DRAWINGS

The invention will be explained in more detail below using an exemplary embodiment. The issued drawings  
20 show:

Figure 1 a schematic definition of a scattering matrix and waves entering and leaving at the two-port and

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Figure 2 a block diagram of a vectorial three-port network analyzer.

Figure 1 shows two-port characterized by its scattering  
30 matrix. The waves  $a_1$  and  $a_2$  are the waves travelling to the two-port and  $b_1$  and  $b_2$  correspondingly the waves propagating in the opposite direction. The following relationship holds true:

$$35 \quad \begin{pmatrix} b_1 \\ b_2 \end{pmatrix} = \underbrace{\begin{pmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{pmatrix}}_{= [S]} \begin{pmatrix} a_1 \\ a_2 \end{pmatrix}$$

The interesting special case of a 3-port network analysis system is illustrated as a block diagram in Figure 2. It can be seen that  $2n = 6$  measurement locations (15) are necessary. Figure 2 demonstrates how such a 5 construction is to be realized, and serves as a basis for the description of the multiport methods.

#### DESCRIPTION OF THE PREFERRED EMBODIMENTS

10 Figure 2 illustrates how the signal from a source 17 is conducted via a changeover switch 16, whose properties, e. g. reproducibility, reflection and long-term stability, therefore do not influence the measurement accuracy, onto the three branches 18, 19 and 20. The measurement location 15, assumed to be ideal, in each case take up a measure of the incoming and transmitted waves. All deterministic non-idealities and incompletenesses in the form of mismatches and crosstalk are combined and taken into account in the error matrices 13, 15 20 14a and 14b. At the ports 10, 11 and 12, the measurement object 21 (DUT) is connected to the vectorial network analyser.

25 The measurement values  $m_n$  for the reflection and transmission behaviour of realized calibration standards are measured in each switch position at two measurement locations each time. For the RRMT according to Claim 1 there are the thru standards of known length and attenuation which are connected between each possible 30 measurement port combination, the match standards and the reflection standards which are similar to short and open circuits, all being measured at n-one-port. As far as one of the other methods of the invention is carried out, these measurement values  $m_n$  are measured with the 35 features as disclosed in the corresponding Claim. The scattering matrix is calculated from these measurement values  $m_n$  as described in the following.

The methods can be subdivided into three steps from the mathematical standpoint:

- 1.: so-called self-calibration of the unknown reflection standards,
- 5 2.: so-called direct calibration and
- 10 3.: system error correction.

In the first step, the unknown parameters in the calibration standards are calculated. Trace and determinant properties of mapping matrices are utilized here, as described in Heuermann, "Sichere Verfahren zur Kalibrierung von Netzwerkanalysatoren für koaxiale und planare Leitungssysteme", [Reliable methods for the calibration of network analysers for coaxial and planar line systems], Dissertation document, Institute for Radiofrequency Technology, Ruhr-University Bochum, 1995, ISBN 3-8265-1495-5. The match calibration standards are not taken into account with ideal properties ( $S_{11} = 0$ ) in the mathematics. This has the effect that the resultant equations for calculating the reflection values of the two R standards are significantly longer. However, these equations do not differ from the customary solutions of self-calibration calculations with regard to above called unambiguity considerations for the line, impedance and reflection standards.

In the case of the second step of direct calibration, the error coefficients are calculated. This is done for the RRMT method according to Claim 1 and for the LRRM method according to Claim 3 using traditional routes of the 10-term methods, as have been described in Schick, "Messsysteme der Hochfrequenztechnik", [Measurement systems of radiofrequency technology] Hüthig-Verlag, Heidelberg, 1984 and Heuermann, "Sichere Verfahren zur Kalibrierung von Netzwerkanalysatoren für koaxiale und planare Leitungssysteme", [Reliable methods for the

calibration of network analysers for coaxial and planar line systems], Dissertation document, Institute for Radiofrequency Technology, Ruhr-University Bochum, 1995, ISBN 3-8265-1495-5. A two-port calibration is carried

5 out for each through connection and the error coefficients are known for this connection. The route for the treatment of the multiport method is then described as the third step.

10 For the methods according to Claims 2 and 4, routes of the 7-term methods for the calculation of the error coefficients are already described in Heuermann, "Sichere Verfahren zur Kalibrierung von Netzwerkanalysatoren für koaxiale und planare Leitungssysteme", [Reliable methods for the calibration of network analysers for coaxial and planar line systems], Dissertation document, Institute for Radiofrequency Technology, Ruhr-University Bochum, 1995, ISBN 3-8265-1495-5 for similar

15 two-port methods. The combination of these results of the two-port methods into a multiport method is likewise explained in the next step.

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**In the case of the third step** for carrying out a system error correction, the measurement data of an unknown

25 measurement object are corrected by the errors of the VNA and the leads.

For the methods according to Claims 1 and 3, which are based on the 10-term principle, the error model in Figure 2 forms the initial basis for the mathematical description of the 10-term multiport methods. For the sake of simplicity, here shall be carried out the mathematical derivation for the measurement of three-ports. This procedure can be generalized to n-ports in

30 a simple manner by providing a changeover switch with n output ports and taking account of two additional measurement locations for each further port of the measurement object.

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In order to determine the traditional error matrices of the 10-term model, a two-port calibration is carried out between each measurement port combination with the error matrices  $[A]$ ,  $[F]$ , and  $[G]$ . The following holds 5 true:  $[F] = [B_I]^{-1}$  and  $[G] = [B_{II}]^{-1}$ .

For the switch position I, the error matrix  $[A]$  is the reference port, containing three error variables, for 10 II it is  $[F]$  and for III  $[G]$ . The two other measurement ports for each switch position contain only the two error variables (e.g.:  $F_T$ ,  $F_L$ ) of the transmission error network. The associated variables are subsequently to be deleted once, twice and three times, depending on the switch position. Consequently,  $3*3 + 3*2*2 = 21$  error 15 variables result for the three-port case.  
The correction calculation of the measured values of the measurement object ( $m_i$ ) using the 21 error variables can be formulated as follows:

20

$$\begin{pmatrix} m'_2 \\ a'_1 \end{pmatrix} = [A']^* \begin{pmatrix} m'_1 \\ b'_1 \end{pmatrix}, \quad b'_2 = m'_4 / F'_T, \quad (2)$$

$$a'_2 = F'_L * b'_2, \quad b'_3 = m'_6 / G'_T, \quad a'_3 = G'_R * b'_3. \quad (3)$$

25 Rearrangement yields 6 equations for the 6 wave variables  $a'_1$ ,  $a'_2$ ,  $a'_3$ ,  $b'_1$ ,  $b'_2$ ,  $b'_3$ .

The procedure is exactly the same for the remaining 30 switch positions. These  $3*6$  equations can be used in the equation

$$\begin{pmatrix} b_1 \\ b_2 \\ b_3 \end{pmatrix} = \begin{bmatrix} & & \begin{pmatrix} a_1 \\ a_2 \\ a_3 \end{pmatrix} \\ Sx & & \end{bmatrix} \quad (4)$$

In this case, the values of a matrix column are obtained for each switch position, which ultimately leads to a system of linear equations comprising two  $n \times n$  measured value matrices and the  $n \times n$  scattering matrix.

5 If this system of equations is resolved with respect to the  $[S_x]$  matrix, then the error-corrected scattering parameters of an  $n$ -port are available.

For the methods according to Claim 2 and 4, which are based on the 7-term principle, the error model in Figure 2 also forms the initial basis for the mathematical description of the 7-term multiport methods. For the sake of simplicity, here also shall be carried out the mathematical derivation for the measurement of three-ports. This procedure can be generalized to  $n$ -ports in a simple manner by providing a changeover switch with  $n$  output ports and taking account of two additional measurement locations for each further port of the measurement object.

20 In order to determine the traditional error matrices of the 7-term model, a two-port calibration is carried out between the reference port with the error matrix  $[A]$  and the error matrices  $[B_i]$  ( $i = 1, 2, \dots, n$ ). The designation 7-term module stems from the fact that the associate  $2 \times 2$  error matrices  $[A]$  and  $[B_i]$  contain a total of 7 error terms since one of the 8 variables contained can always be set to 1.

25 It is subsequently advantageous to formulate the mathematical formulation of the two-port model in the inverse form of the transmission parameters specified:

$$[G] = [A]^{-1}, [H_i] = [B_i]^{-1}, i = 1, 2 \quad (2)$$

35 where the following holds true for the inputs and outputs at the error networks:

$$\begin{pmatrix} b_1 \\ a_i \end{pmatrix} = [G]^* \begin{pmatrix} m_1 \\ m_2 \end{pmatrix} , \quad \begin{pmatrix} a_i \\ b_i \end{pmatrix} = [H_i]^* \begin{pmatrix} m_{2i-1} \\ m_{2i} \end{pmatrix} \quad (3)$$

These equations can be resolved with respect to the  $a_i$   
5 and  $b_i$

$$\begin{pmatrix} b_1 \\ b_2 \\ b_3 \end{pmatrix} = \begin{bmatrix} & & \begin{bmatrix} a_1 \\ a_2 \\ a_3 \end{bmatrix} \\ Sx & & \end{bmatrix} \quad (4)$$

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tem of linear equations comprising two  $n \times n$  measured  
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15 system of equations is resolved with respect to the  
[Sx] matrix, then the error-corrected scattering pa-  
rameters of an n-port are available.

Calibration method for carrying out multiport measurements on semiconductor wafers

List of reference symbols

5

- 10 Port
- 11 Port
- 12 Port
- 10 13 Error matrix
- 14a Error matrix
- 14b Error matrix
- 15 Measurement location
- 16 Changeover switch
- 15 17 Source
- 18 Branch
- 19 Branch
- 20 Branch
- 21 Measurement object

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